

Modeling and Simulation to Predict Split Tensile strength of Concrete Pavement Modified with Silica and Super Plasticizers

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ABSTRACT

This paper expresses the tensile strength from concrete pavement formation under influences of silica and plasticizers, the study monitor tensile behavior from concrete pavement to determine its rate of fracture mechanism of hardened concrete. It defines the definite strength of hydrated cement paste including similar brittle. The study express linear trend from different tensile strength of concrete pavement, maximum tensile strength were observed in ninety days of curing age, the tensile strength experienced variations influences from other concrete characteristics, this will always avoid defects that will lead to high stress concentrations on most of these materials subjected to load that experiences very high stress. The study were monitored under the influences of variation of water cement ratios, increase in tensile strength were observed due to reduction of water cement ratios, while decrease were also experienced due to increase in water cement ratios, the study explain the effect on void ratios and concrete porosity, it definitely evaluates the rate of heterogeneity in the materials that must be observed thoroughly in mix design, if the required tensile strength of concrete can be achieved. The developed model simulation values were subject to validation, and both parameters generated best fits correlation.

Keywords: Modeling Split Tensile Concrete Pavement Silica and Plasticizers

INTRODUCTION

Tensile Strength concrete that plays an essential role in the fracture mechanism of hardened concrete was express by (Guang li 2004). These explained definite strength of hydrated cement paste or of similar brittle (Mindess et al. 2002). Hydrated cement paste are known to contain several discontinuities – pores, micro cracks and voids, but the exact apparatus source that affect overall strength is not known (Ode and Eluozo 2016a).

It is noted that the voids themselves need not act as flaws, because it has been observed that the flaws may consist of cracks in its individual crystals, these are known to be associate with the voids, it also be caused by shrinkage or poor bond. Cement and aggregates, these are the most indispensable constituents materials that are applied in concrete production, they are important materials required in the construction industries. This has led to an interrupted and increasing demand of natural constituents used for their production (Guang li 2004Ode and Eluozo 2016bOde and Eluozo 2016c). Several researches on application material for partial replacement such as of waste tyres as fine and coarse aggregates are available in the literature

of (Eldin and Senouci, 1993; Topcu, 1995; Toutanji, 1996; Khatib and Bayomy, 1999; Ling, 2011; Ohemeng and Yalley, 2013Ode and Eluozo 2016d), they demonstrated the feasibility applying gargantuan amounts of waste tyre in concrete materials. Furthermore plastic densities of concrete are projected to be lowered than ordinary concrete due to the low specific gravity of plastics. Al-Manager and Dalal (1997) explained that bulk density of plastic concrete observed decreased as the plastic content experiences increased. Suganthy et al. (2013) also explained decreased in weight of concrete as the plastic content observed increased. The study also projected linear relationship between decrease in weight and increase in plastic content. Batayneh et al. (2007) also explained the integration of ground plastic in concrete that influences its compressive strength. Naik et al. (1996) examined the effect of post-consumer waste plastic in concrete as a soft filler. The test results explained lower compressive strength of the mix modified with plastic compared to reference mixture without plastic. Choi et al. (2005) also observed a reduction in both compressive strength and splitting tensile strength Marzouk (2007Ode and Eluozo 2016e; Ode and Eluozo 2016fOde and Eluozo 2015) further study carried out also explained the

reduction of compressive strength in plastic concrete when the sand was replaced by plastic. Al-Manasser and Dalal (1997) again studied that affect plastic on concrete mix observed similar direction. It was noticed that the splitting tensile strength decreased as the plastic content increased. Batayneh et al. (2007) also reported that the splitting tensile strength and the flexural strength of concrete mix slumped as the plastic content went up (Ode 2004).

THEORETICAL BACKGROUND

Nomenclature

- α = Constant
- C = Split Tensile Strength
- $A_{y(1-n)}$ = water cement Ratio
- U^2 = Cementious Material/Additive's
- B_y = Slump /Specific Gravity
- Y = Curing Age

$$\frac{dC}{dy} + A_{(y)}C_{(d)} = B_{(y)}C_d^n; n \geq 2 \dots \dots \dots (1)$$

Divided by (1) through by C_d^{-n} we have obtain

$$C_d^{-n} \frac{dC}{dy} + A_{(y)}C_d^{1-n} = B_{(y)} \dots \dots \dots (2)$$

Let $\alpha = C_d^{1-n}$

$$\frac{dC}{dy} = (1-n)C_d^{-n} \frac{dC}{dy}$$

Multiplying Equation (2a) through by (1-n)

$$(1-n)C_d^{1-n} \frac{dC}{dy} + (1-n)A_{(y)}C_d^{1-n} = (1-n)B_{(y)} \dots \dots \dots (3)$$

Let $\frac{2}{2-\alpha} = U^2$

$$C = \frac{1}{U^2} \int (1-n)B(y)dy = \frac{1}{U^2} (1-n)B(y)Y + K_1 \dots \dots \dots (4)$$

$$\left[C = \frac{(1-n)}{U^2} B(y)Y \right] \dots \dots \dots (5)$$

MATERIALS AND METHOD

Flexural and Tensile Strength

Concrete has relatively high compressive strength in the range of 10 to 50 Nmm² and 60 to 120 Nmm² for high strength concrete. Tensile strength significantly low constitutes about 10% of the compressive strength (Neville & Brooks, 1996; Popovics, 1998).

Flexural test is done to find out the tensile strength of concrete. A typical set up recommended by British Standard is illustrated in Figure 3.1.

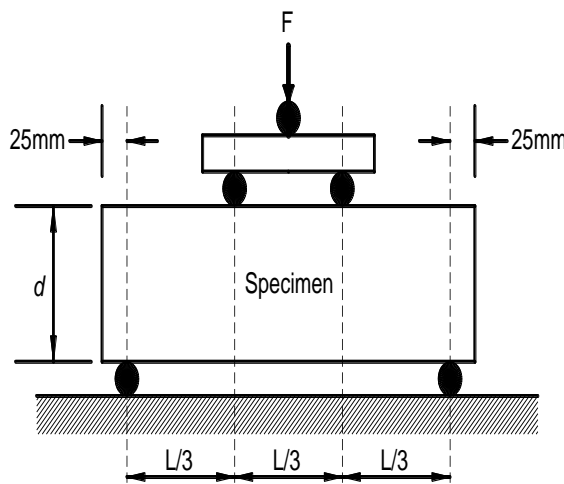


Fig 3.1 Flexural Beam Test Set-ups

From Mechanics of Materials and analysis of Figure 3.1, maximum tensile stress is expected to occur at the bottom of the constant moment region within which pure bending occurs.

The modulus of rupture can be calculated as:

$$f_{tb} = \frac{FL}{bd^2} \text{ Where}$$

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L=Span of specimen beam

F=maximum applied loads

b=breadth of beam

d=depth of beam

Other method used in determining the tensile strength of concrete is the indirect tension test

The splitting tensile strength is calculated using the stated formula

$$F_{st} = \frac{2P}{\pi LD} \text{ Where}$$

(split cylinder test or Brazilian test, Figure 2.3)

BS 1881: Part 117:1983 and ASTM C496-71.

As recommended in these standards, the splitting test is done by applying compression loads at a loading rate 0.0112 to 0.0231 MPa/s along two axial lines that are diametrically opposite on a specimen 150 x 300 mm cylinder.

L=Length of Cylinder

P=Maximum applied loads

D=Diameter of Cylinder

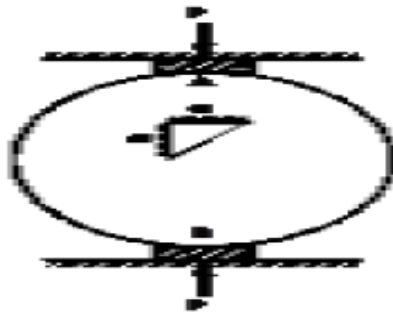


Fig 3.2 Tensile splitting Analysis

RESULTS AND DISCUSSION

Table: 1 Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

Curing Age	Predictive Values for Split Tensile Strength of Concrete Pavement (W/C of 0.23)	Experimental Values for Split Tensile Strength of Concrete Pavement (W/C of 0.23)
7	1.10314057	1.1032
14	2.20628114	2.2064
21	3.30942171	3.3096
28	4.41256228	4.4128
35	5.51570285	5.516
42	6.61884342	6.6192
49	7.72198399	7.7224
56	8.82512456	8.8256
63	9.92826513	9.9288
70	11.0314057	11.032
77	12.13454627	12.1352
84	13.23768684	13.2384
90	14.1832359	14.184

Table: 2 Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

Curing Age	Predictive Values for Split Tensile Strength of Concrete Pavement (W/C of 0.30)	Experimental Values for Split Tensile Strength of Concrete Pavement (W/C of 0.30)
7	1.002855063	1.0031
14	2.005710126	2.0062
21	3.008565189	3.0093
28	4.011420252	4.0124
35	5.014275315	5.0155
42	6.017130378	6.0186
49	7.019985441	7.0217

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56	8.022840504	8.0248
63	9.025695567	9.0279
70	10.02855063	10.031
77	11.03140569	11.0341
84	12.03426076	12.0372
90	12.89385081	12.897

Table: 3 Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

Curing Age	Predictive Values for Split Tensile Strength of Concrete Pavement (W/C of 0.35)	Experimental Values for Split Tensile Strength of Concrete Pavement (W/C of 0.35)
7	0.931222558	0.931
14	1.862445116	1.862
21	2.793667674	2.793
28	3.724890232	3.724
35	4.65611279	4.655
42	5.587335348	5.586
49	6.518557906	6.517
56	7.449780464	7.448
63	8.381003022	8.379
70	9.31222558	9.31
77	10.24344814	10.241
84	11.1746707	11.172
90	11.97286146	11.97

Table: 4 Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

Curing Age	Predictive Values for Split Tensile Strength of Concrete Pavement (W/C of 0.40)	Experimental Values for Split Tensile Strength of Concrete Pavement (W/C of 0.40)
7	0.859590053	0.8596
14	1.719180106	1.7192
21	2.578770159	2.5788
28	3.438360212	3.4384
35	4.297950265	4.298
42	5.157540318	5.1576
49	6.017130371	6.0172
56	6.876720424	6.8768
63	7.736310477	7.7364
70	8.59590053	8.596
77	9.455490583	9.4556
84	10.31508064	10.3152
90	11.05187211	11.052

Table: 5 Predictive Values of Split Tensile Strength Varying at Different water cement ratios

Curing Age	0.23	0.3	0.35	0.4
7	1.103141	1.0028551	0.931222558	0.859590053
14	2.206281	2.0057101	1.862445116	1.719180106
21	3.309422	3.0085652	2.793667674	2.578770159
28	4.412562	4.0114203	3.724890232	3.438360212
35	5.515703	5.0142753	4.65611279	4.297950265
42	6.618843	6.0171304	5.587335348	5.157540318
49	7.721984	7.0199854	6.518557906	6.017130371
56	8.825125	8.0228405	7.449780464	6.876720424
63	9.928265	9.0256956	8.381003022	7.736310477
70	11.03141	10.028551	9.31222558	8.59590053
77	12.13455	11.031406	10.24344814	9.455490583
84	13.23769	12.034261	11.1746707	10.31508064
90	14.18324	12.893851	11.97286146	11.05187211

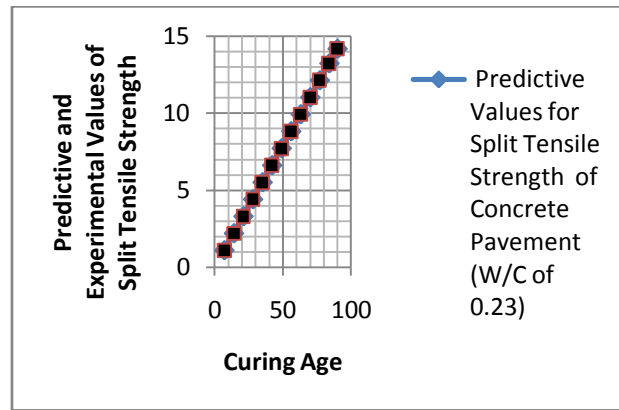


Fig1. Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

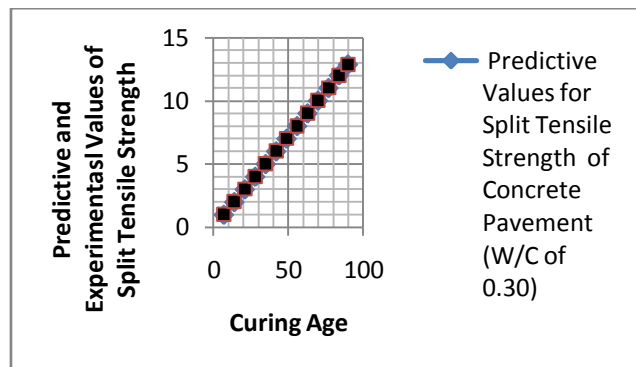


Fig2. Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

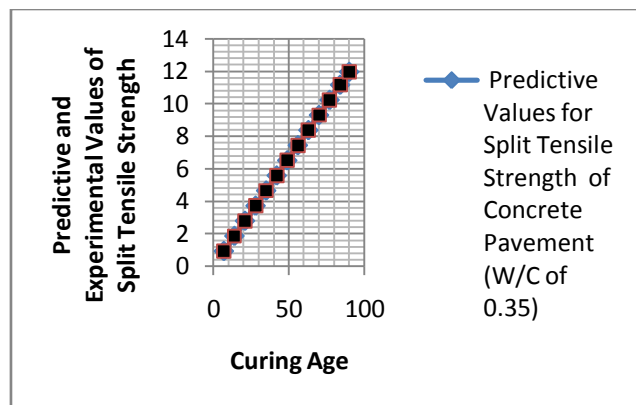


Fig3. Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

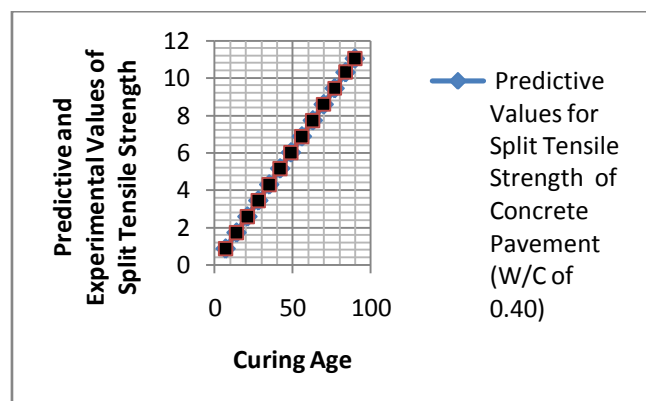


Fig4. Predictive and Experimental Values of Split Tensile Strength at Different Curing Age

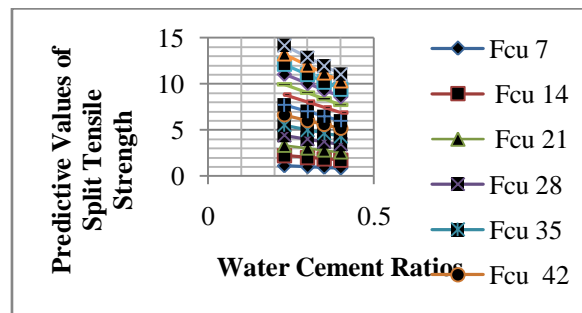


Fig5: Predictive Values of Split Tensile Strength Varying at Different water cement ratios

Figure one to five shows the trend exhibited by the tensile strength of the materials, linear trend was observed in all the figures, but the tensile parameters experience variation since, the tensile strength of concrete definitely plays essential roles in the fractural mechanism of any hardened concrete. This implies that definite strength from hydrated cement paste experiences similar brittle. This has been an accepted assessment that explained fracture in concrete; this arises through its cracking. This implies that concrete fracture is fundamentally a tensile failure irrespective of whether the fracture is prompted by compression, it definitely exhibits its behavior from concrete including loading mechanisms).Freezing internal expansion, or by other factors.

The study experienced concrete characteristics influence that subjected the behavior of the material to experience these required results presented in the figures, change in tensile are observed also in the figures base on some factors, the concrete making procedure, such as batching, mixing, delivering, placing, and consolidation of fresh concrete, testing procedure, including the shape and size of the specimen such as preparation method, type of test machine, and rate of loading, age at testing, effectiveness and duration of curing Age, more so curing temperature, Air content and porosity, Moisture Content, the behave of tensile strength of any model concrete maintained these stated principals, such conditions were considered in the study that allowed the tensile parameter including its behavior as it is observed from the graphical representation, the developed parameters from simulation values were compared with experimental values, and both parameters observed best fits correlations

CONCLUSION

The study has observed the behavior of the materials on the development of tensile strength, these implies that the materials applied will definitely determine the type of tensile that is

generate from the study, in most conditions the defects that lead to high stress concentrations on most of these materials are subjected under load as it experience every high stress.

It is normally experiences reach in very small volumes of the specimen; these result generated are from the microscopic fracture, while the average (normal) stress in the whole specimen is comparatively low. Consequently, it is observed that mechanical properties of hardened concrete are controlled to a large extent based on the fact that its tensile strength is just only precisely one-tenth of its compressive strength. Therefore, the mechanisms of tensile strength including its rate of failure are observed to play major role in strength variation and development of the materials. Since tensile strength of concrete is lower than its compressive strength due the ease with which cracks can propagate under tensile loads. Tensile strength of concrete is known to be considered in design, it is normally assumed to be zero.

However, it is an imperative property because cracking in concrete is usual due to tensile stresses induced by loads applied, this include the deterioration mechanisms factors, or that of environmental variations, tensile strength development from the concrete material was monitored under the influence of variation of water cement ratios, the increase of tensile strength were experienced based on reduction of water cement ratios, while decrease in tensile strength were observed based on increase in water cement ratios, other influential factors includes variation of porosity and void ratios in concrete and its concrete placement. The developed simulation values were compared with experimental parameters and both results developed best fits correlation

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